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FEBRUARY 15, 1917

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Vol. II

February 15, 1917

No. 2

EVERY STRONG President Wilson selected diplomatic relations with Germany it has been apparent that this country has been on the brink of war. It is not prepared to face a war in the air. It is not too late that hysterical appeals for more aviation be allowed to confuse the situation and to divert the attention of the public from the real aeronautical need of the United States which is for more types of planes, especially for more fighting planes, scouts, pursuit machines, long-range reconnaissance machines, crossed airplanes and bombers.

American training machines are the equals of any in the world. The fact that we are building good training machines gives promise for the future, but the true diplomatic situation rather the fact that we shall probably have some good machines for military and naval work a year from now seems of very little importance. American airplane workmanship can attain the highest standards, but the training machine type is not useful in war.

Today neither the United States Army or Navy can obtain immediately airplanes fit to cope with the military machines that are in daily use abroad. It is no promise that we should hasten the development of military airplanes for army and naval use, but there is very little prospect that we shall have such machines in any considerable quantities for some time to come.

No one is to blame for this situation except the legislators in Congress, who, up to last August refused repeatedly to appropriate the substantial sums of money without which it was impossible to expect that the airplane industry in this country would flourish.

The fact that large appropriations for both the Army and Navy were made last August, so that the two branches of the service had altogether in the neighborhood of \$17,000,000 at their disposal for the current fiscal year, has not helped matters in any great extent insofar as the immediate deliveries of battleplanes are concerned.

The development of an aerobically engine is a matter of a year at least. That we have a number of satisfactory engines of 150 horsepower and less is an immense step in advance of the situation that existed a year ago but it is due almost as much to the hope on the part of the manufacturers that they would be able to sell abroad as it is to the stimulation of the appropriations of last August. The results of the encouragement which that appropriation gave to the industry will not become fully available for six months more at least, and it

would be unreasonable to expect engines of greater horsepower to reach a production basis until then.

Now that we have the engines we have only just begun to solve the problems of military aviation. No designer can begin to draw up plans for an airplane until he has determined upon the engine which is to go into it. It is now necessary to begin to build planes around the engines that have only just been perfected. This is a work that will require at least another year of intensive development and experimental flying before the solution is approached.

Any visitor to the recent Aeronautical Exposition who did not gain an appreciation of the fact that the design of an airplane is a delicate engineering problem requiring months of careful thought and experimentation failed to grasp the chief lesson of that exposition.

The United States Army has suggested that the so-called two plane reconnaissance tractor is a false development. It may be valuable against an enemy who has no airplanes, but against an enemy who is prepared it has practically no military or naval value. Yet that was almost the only type of machine which the constructors found available for exhibition.

The United States Navy has asserted that it needs machines of great weight-carrying ability and large fuel-carrying capacity. No such machines were shown. The pressing need of today is not only for more thoroughly trained aviators, it is for more machines and more types of machines. Whenever the constructors are in a position to deliver military types of airplanes in quantities, the country will have the aviators to fly them.

The personnel and material problems both need to be solved. The personnel problem is comparatively easy of solution because so long as the attraction of flying as an adventure remains, there will be no lack of young men who are willing to learn to fly at the Government's expense. But there is no one in training civilians to fly unless some possibility exists of fitting the aviators out with fighting machines when war comes.

The Cover Photograph

The cover of this issue shows the first airplane to fly, the original Wright machine of 1903, restored to the condition in which the Wright Brothers used it. Orville Wright and Glen L. Martin are in front of the plane and between them is the Michoud trophy, won by the late Wilbur Wright in France in 1906 for a flight of 77 miles in 2 hours and 20 minutes.

The Venturi Tube

By Winslow H. Herschel

of the Bureau of Standards

Boards* used a Venturi tube as an anemometer in tests, and it has been used more recently as a speed indicator on airplanes. A Venturi tube consists of a converging cone, forming a nozzle of approximately the shape of a cone, tapered, followed by a diverging cone, usually with a short cylindrical throat between the two. The diverging cone has a small angle, about 3 degrees, so as to reduce the friction loss to a minimum. The difference between the pressure at the upstream end of the converging cone, and at the throat, is a measure of the velocity.

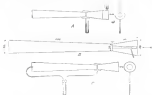


FIG. 3. TYPES OF VENTURI TUBES
(a) SIMPLE VENTURI TUBE; (b) AND (c) ADVANCED TYPES; (d) AND (e) ADVANCED TYPES.

When the Venturi tube is inserted as an index of a part line, and is used to measure discharge, this principle is expressed in terms of water volume, and known as the "head on Venturi," indicates the velocity through the throat. For the present purpose it seems preferable to find the velocity at the upstream end, which is more nearly equal to the desired velocity of flight.

Let p , ρ , and v , be the pressure, density and velocity, respectively, at the upstream end where the section is A , and let p_t , ρ_t and v_t represent the same quantities at the throat, where the section is A_t . Assuming adiabatic expansion, the well-known formula of the Saint-Venant will apply:

$$\frac{p}{\rho} = \frac{p_t}{\rho_t} \left(1 - \frac{v_t^2}{v^2} \right) \quad (1)$$

where v is the ratio of specific heats, γ , which may be taken as 1.4 for air. This formula may also be applied to pitot tubes, in place of equation (1) — $A = \sqrt{\frac{p}{p_t}}$, but the increase in accuracy is not sufficient to compensate for the greater complexity.

Since $A = \frac{v}{v_t} = \frac{A_t}{A}$, and therefore $\frac{A}{A_t} = \left(\frac{p}{p_t} \right)^{\frac{1}{\gamma}}$ and $\frac{A}{A_t} = \left(\frac{p}{p_t} \right)^{\frac{1}{\gamma}}$ (2)

For dry air, at a temperature of 70 degrees Fahrenheit (21 degrees C.) Equation (1) may, with the help of Equation (2), be reduced to:

$$v = 322 \sqrt{\frac{p}{p_t}} \quad (3)$$

where the coefficient, 322, is equal to $\sqrt{\frac{2 \times 144}{1.4 \times 32.2 \times 1000}} \times 1000$ in English units.

In using equation (3), equation (2) is unchanged, since the coefficient has a value of 108.7 to give velocity in meters per second.

TABLE I
THEORETICAL HEADS ON VENTURI TUBES FOR TEMPERATURES OF 0, 10, 20, 30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150, 160, 170, 180, 190, 200, 210, 220, 230, 240, 250, 260, 270, 280, 290, 300, 310, 320, 330, 340, 350, 360, 370, 380, 390, 400, 410, 420, 430, 440, 450, 460, 470, 480, 490, 500, 510, 520, 530, 540, 550, 560, 570, 580, 590, 600, 610, 620, 630, 640, 650, 660, 670, 680, 690, 700, 710, 720, 730, 740, 750, 760, 770, 780, 790, 800, 810, 820, 830, 840, 850, 860, 870, 880, 890, 900, 910, 920, 930, 940, 950, 960, 970, 980, 990, 1000, 1010, 1020, 1030, 1040, 1050, 1060, 1070, 1080, 1090, 1100, 1110, 1120, 1130, 1140, 1150, 1160, 1170, 1180, 1190, 1200, 1210, 1220, 1230, 1240, 1250, 1260, 1270, 1280, 1290, 1300, 1310, 1320, 1330, 1340, 1350, 1360, 1370, 1380, 1390, 1400, 1410, 1420, 1430, 1440, 1450, 1460, 1470, 1480, 1490, 1500, 1510, 1520, 1530, 1540, 1550, 1560, 1570, 1580, 1590, 1600, 1610, 1620, 1630, 1640, 1650, 1660, 1670, 1680, 1690, 1700, 1710, 1720, 1730, 1740, 1750, 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Average Values for Machines Over 2500 Pounds Weight

This group is composed of excellent, creditable machines. Very similar to observation. It is therefore possible to draw some fairly definite conclusions.

(a) Average gross weight, 2957 pounds.
(b) Average wing area, 493 square feet.
(c) Average horsepower, 130. The latter figure is undoubtedly increased by the inclusion of the Curtiss R-4 with its 200 horsepower engine. There is a tendency to give higher power to this class with correspondingly better performance.
(d) Average maximum speed, 55 miles. This figure is probably a very fair index of the machine's possible top speed (it is to be maintained). It should be noted that it would be possible to take up much higher speeds, but not decrease the speed, in fact, to increase it slightly. At the same time, maximum speed would be increased.

(e) Average weight per horsepower, 18.4 pounds. The Curtiss lowest the average value, and as an indication of what will follow when higher engine speeds, such as the new Thomas and Brownlow, enter into construction.

(f) Average weight per square foot of wing area, 5.99 pounds.

(g) Average maximum speed, 56.24 miles per hour.
Average maximum speed, 45.52 miles per hour.
Average climb in 10 seconds, 3660 feet.

The number of machines considered is too small for curves to be plotted, but it is interesting to see how in diminishing the weight per horsepower from 24.2 pounds to 19.21 pounds the maximum speed increases from 44 to 60 miles per hour, while the low observed wing loading gives a loading speed of 42 miles per hour as compared with the Curtiss of 50 miles per hour.

(h) Average ratio of span span = 1.34.

This is an important point to be considered in the design of a machine. As we shall see later in considering longitudinal stability, it is quite possible to secure effective static stability by using a short body with a large tail surface placed at a negative angle. But an excessively short body, although it means saving in weight, may fail to give dynamic stability, due to lack of damping. At this stage of the survey, we can only fix on a length for the body in taking on a machine such as the above.

(i) Average upper ratio upper wing, 7.70.

These series, in the light of these figures, furnish why an aspect ratio of 7.5 for the upper wing, and 7.5 for the lower should not be necessarily employed.

(j) Gap between ratio is generally 1.00 in every case. Without undue reason, it would appear that for the machine of this size, the increased structural weight of a large gap between ratio is prohibitive, whereas in smaller machines with smaller loads, much greater values might be employed to advantage.

The dimensions at control and stabilizing surfaces present an exceedingly complex problem, so much further being involved. This will be naturally studied in our design, but in the preliminary stages some of the following empirical relationships may be useful.

(k) Aspect or wing flap area. The dimensions of these are may be necessary, in connection, in the weight and lateral ratios of gyration of the machine and on the span of the wings which gives the increased arm of the ailerons. These ratios are too complex, however, and at present the following formula offers a fairly satisfactory standard of comparison:
 $(S_{a1} + S_{a2}) = CL$, where S = area of wings, S_1 and S_2 = areas of upper and lower wings, a = average aspect of upper and lower wings, L = wing chord. Where C is large there is powerful lateral control, where C is small there is weak lateral control. The values for the above five machines are as follows:

Wright	Curtiss	Wright-Martin	Alcock	Wright-Martin
7.45	7.45	7.45	7.45	7.45

The powerful lateral controls (recent definition in handling just as too weak controls. The average value of $C = 5.28$ might be at least some guide.

(l) For the horizontal design and stability, the following very rough formula is sometimes employed in preliminary work, based on other variables to those mentioned in the previous paragraph:
 $a = \frac{W}{L}$, where a = wing constant, W = area of elevator and stabilizer, L = overall length, b = area of wings and t = mean chord.

The following constants hold for our five well controlled machines:

Wright	Curtiss	Wright-Martin	Alcock	Wright-Martin
0.00	0.00	0.00	0.00	0.00

These constants are fairly close together, with an average value of .000. A big value of a means powerful control. Without further analysis, it is seen from Table 1 that the stabilizer is much between 20 to 30 per cent larger than the elevator.

(m) Similarly for vertical surfaces, $a = \frac{W}{L}$, where f = constant, L = vertical area of stabilizer and f , L = length, a = area of wings and a = mean span of wings, we find:
Wright-Martin 4.000, Wright-Martin 4.000, Wright-Martin 4.000, Wright-Martin 4.000, Wright-Martin 4.000.
Average value 4.000.

We shall discuss the problem of vertical fin and rudder area more clearly later.

Primary and Advanced Training Airplanes

In the training of military pilots, considerable methods are now employed in the equipment of schools, and there are two distinct types, "primary" and "advanced" training.

The first group, primary, the second group, advanced, is first of all, one of the most important of this type, toward a study, when type of machine in which it is used to acquire confidence in the advanced machine is usually distinguishable from the first machine (primary), although it is somewhat slower. In the second group, an "Advanced" airplane, the first group, advanced, are made for these two types, which are of advanced and primary in design.

(n) Average ratio of span span = 1.34.

Wright-Martin	Curtiss	Wright-Martin	Alcock	Wright-Martin
7.45	7.45	7.45	7.45	7.45

In discussing training machines, there is no other like the of machine, especially in the design of the Signal Corps (Aeronautical Engineering, Nov. 1910 and 1911). These specifications are really obtainable, but some of the most points are set forth here, as they will be applicable to our design of a standard machine, and need be mentioned here in mind by the designer.

IMPORTANT POINTS IN SPECIFICATIONS FOR 1910 AND 1911 FOR MILITARY TRAINING AIRPLANES

Primary	Advanced
1. Trained to be used for:	1. Trained to be used for:
(a) Training and transport	(a) Training and transport
(b) Training and transport	(b) Training and transport
(c) Training and transport	(c) Training and transport

2. Curtiss should be faster 100 to 200 horsepower in 1000 feet, in 1000 feet, or as specified. Machine made in 1000 feet, 1000 feet, or as specified. Machine made in 1000 feet, 1000 feet, or as specified.

3. Minimum speed 20 miles per hour. Maximum speed not less than 40 miles per hour. Minimum speed not less than 20 miles per hour. Maximum speed not less than 40 miles per hour.

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1999-2000, 2000-2001, 2001-2002

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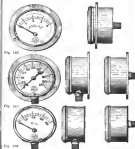
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